

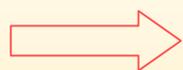
ON-LINE STRAIN AND DAMAGE ASSESSMENT OF ROTORCRAFT STRUCTURAL COMPONENTS



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- One approach would be to use a universal sensor to monitor strain and damage in various materials

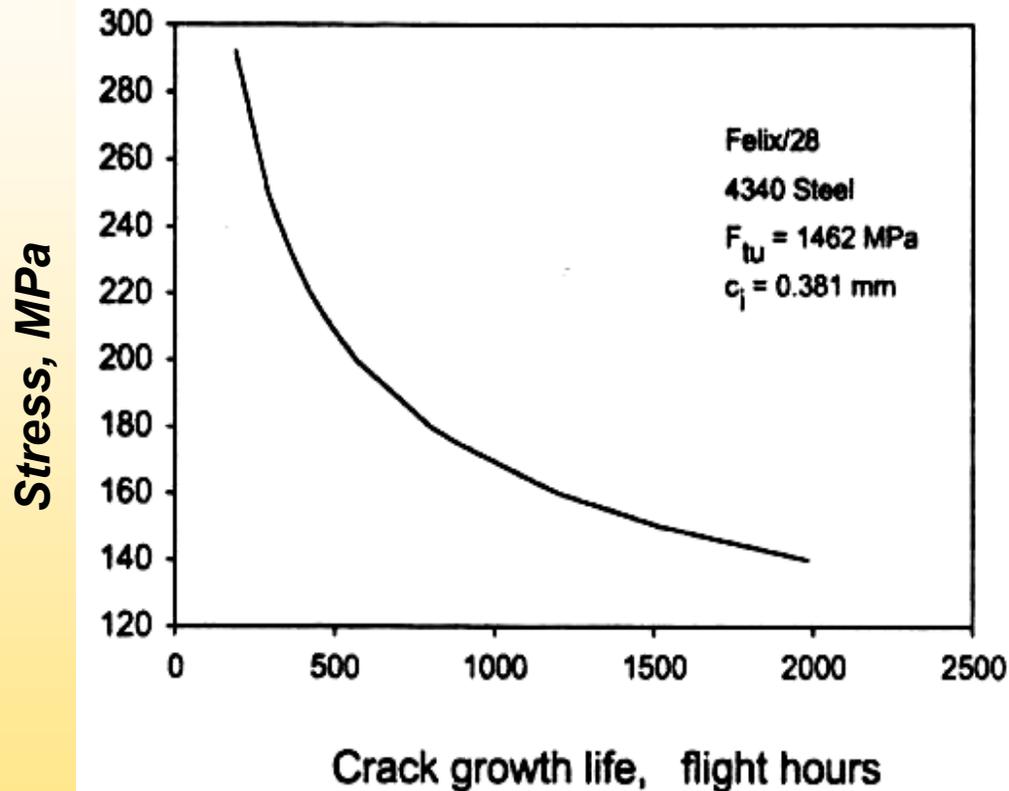


This approach will not work for rotorcraft health monitoring
(Health monitoring of rotorcraft metallic components requires a much higher resolution than that required fixed-wing aircraft)

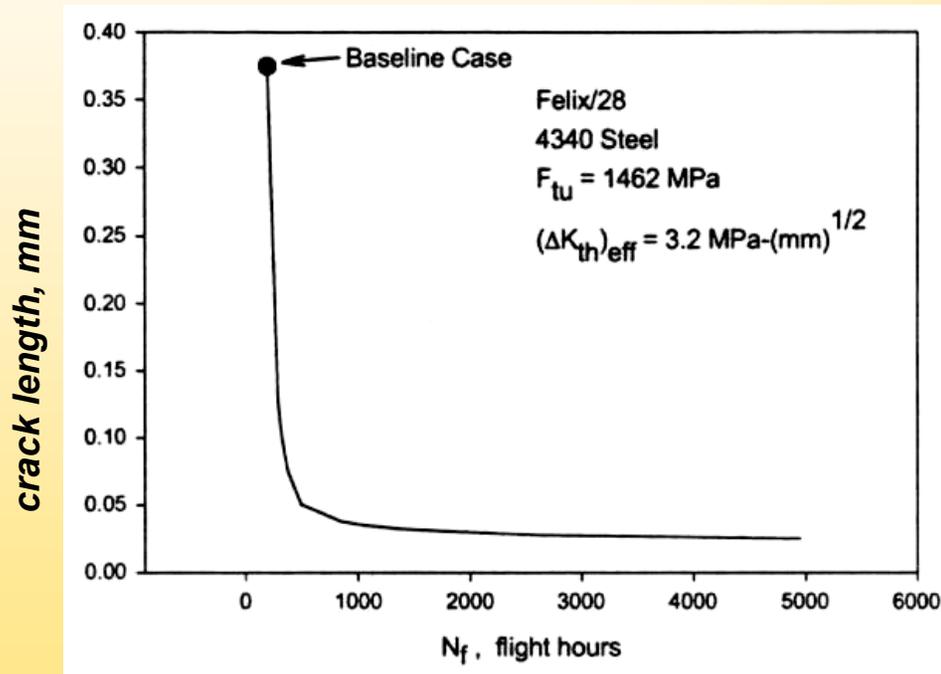
- **Modular approach:** select the sensor type based upon the type of material to be monitored and the resolution required
 - High resolution, proven ACPD technology will be used for detection and monitoring of strain and crack growth in metallic structures
 - Embedded sensor arrays for high frequency vibration monitoring of larger scale, distributed damage in composite structures
- Risk assessment (e.g., sensor failure)



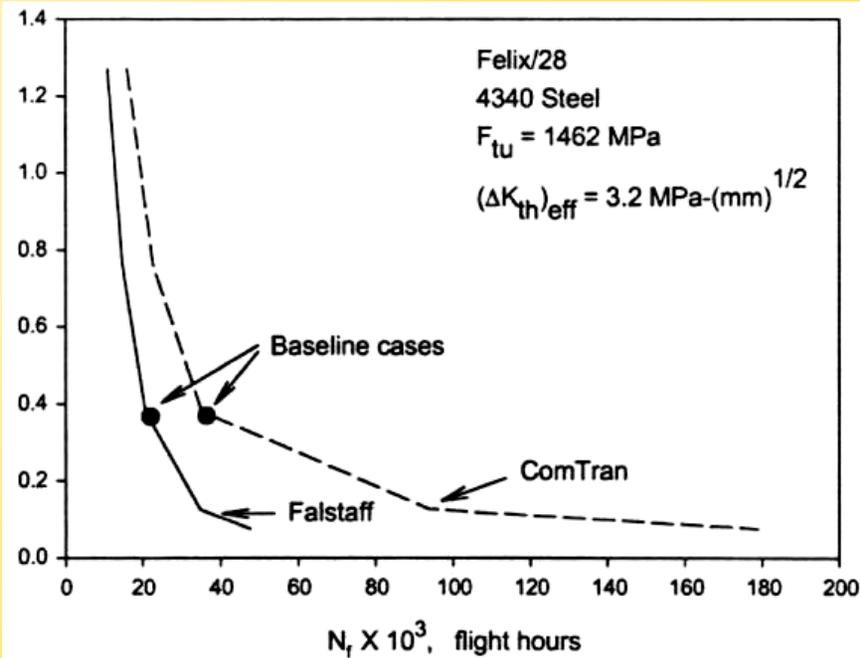
Background



**Crack-growth time-to-failure
(data from Everett, 2002)**



**Crack length vs. flight hours
(rotorcraft) Everett, 2002**



**Crack length vs. flight hours
(fixed-wing) Everett, 2002**



Background



Load Spectra	Material		
	4340 Steel	7075-T6 Aluminum	Ti-6Al-4V Titanium
Felix/28	189 hrs.	146 hrs.	357 hrs.
Falstaff	20,670 hrs.	18,523 hrs.	55,705 hrs.
Comtran	35,214 hrs.	28,453 hrs.	121,811 hrs.
Full Felix	25 hrs.		

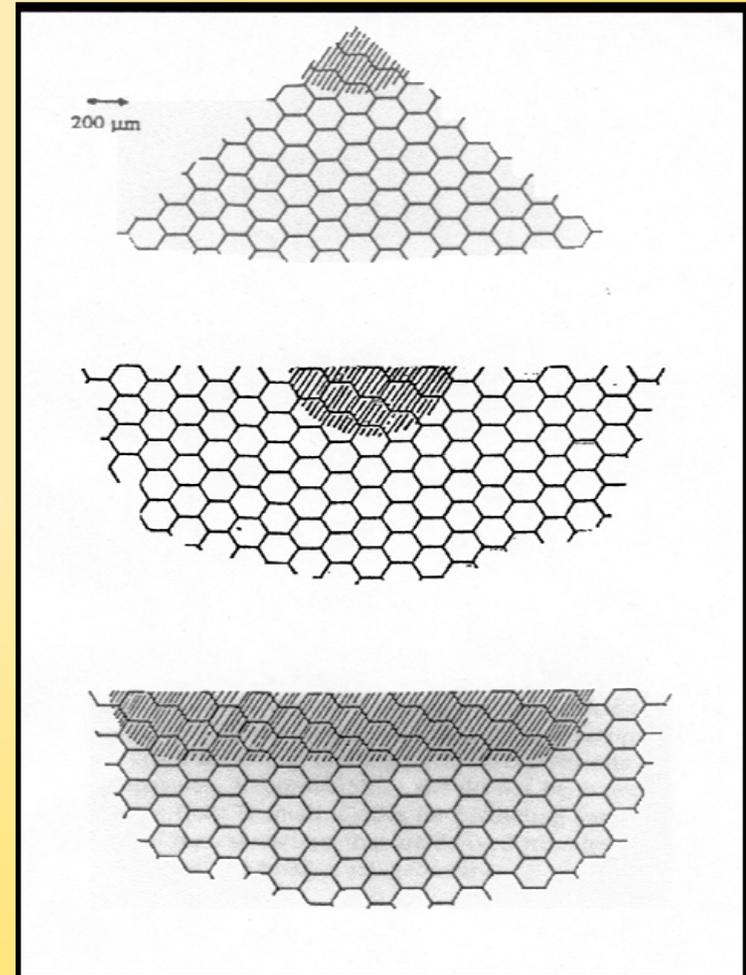
- **If a total life approach is used (with initial flaw size of 30 μm), the life estimate (Felix/28) for 4340 steel increases to 1183 h (versus 189 h if an initial defect size of 0.38 mm is assumed)**
 - **The total life approach requires very accurate monitoring of small cracks at critical locations**
 - **This type of resolution is only attainable using ACPD techniques**



Small Crack Problem (Fatigue Life Prediction)



- *1 to 10 grains*
- *Growth at smaller S.I.F.'s and at faster rates than equivalent long cracks*
- *Scatter significantly greater than that for long cracks*
- *Growth-arrest*
- *Coalescence of micro-cracks*





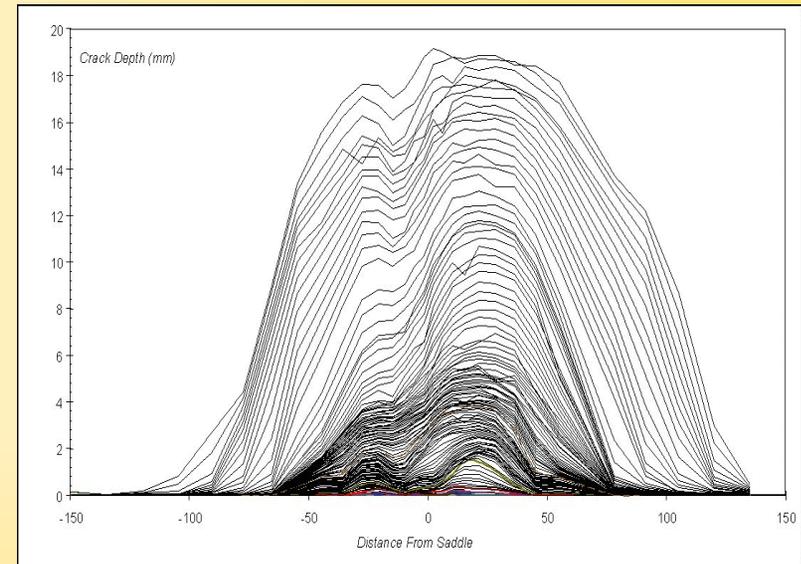
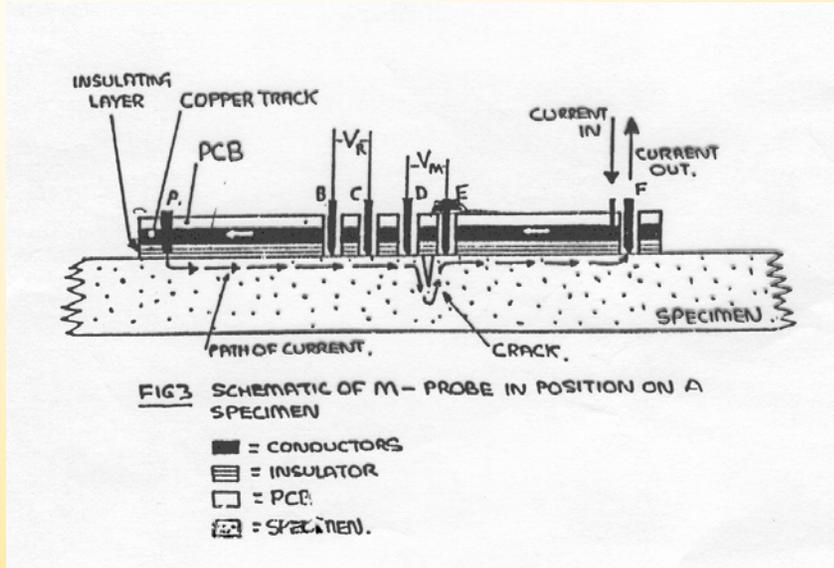
- **Both ACPD and Eddy Current (EC) methods are electromagnetic based**
 - **Measure disturbances to the passage of current in a solid**
 - **Strain changes the resistivity**
 - **Flaws/cracks modify the path of the current flow**
 - **Eddy current techniques rely upon currents induced by a magnetic field**
 - **induced current depends upon properties of the solid, coil geometry, distance between coil and surface**
 - **for paramagnetic alloys (e.g., Al, Ti), induced current densities are very small**
 - **volume into which the current is being induced is often unknown**
 - **if a corner or change in geometry is present e.g., bolt hole or curvature), current density becomes highly disturbed (edge effect)**
 - **changes in geometry can cause lift-off effect (distance between coil and surface changes)**



- **ACPD directly injects current into a material**
 - **allows much higher current densities and increased resolution**
 - *for a given frequency current densities in Al & Ti are approx. 10^3 higher than with eddy current approaches*
 - **even small disturbances can be detected**
 - **surface finish is not an issue – as with eddy current techniques**
 - **Amplitude of injected current density in part is known and is independent of properties of the part**
 - **With current focusing, the current distribution can be further confined which allows highly precise monitoring of bolt holes, notches, bends, etc. in a structure). No edge-effect of lift-off.**



AC Potential Drop



- *An alternating current is injected into a metal surface and flows across defects. A contacting voltage probe is deployed on the surface. Voltage readings are used to calculate crack depth*



AC Potential Drop



- *Only method proven capable of detecting small cracks (10 to 50 μm) and monitoring both small and large crack growth in metals. Provides real-time strain monitoring for overload warning.*

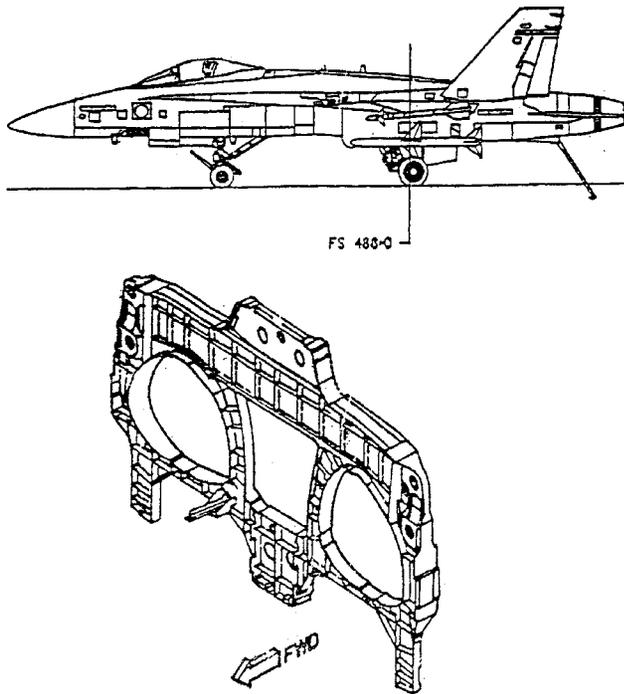


Figure 4.1 Schematic showing the bulkhead 488 and the location of bulkhead 488 in a CF-18 aircraft.

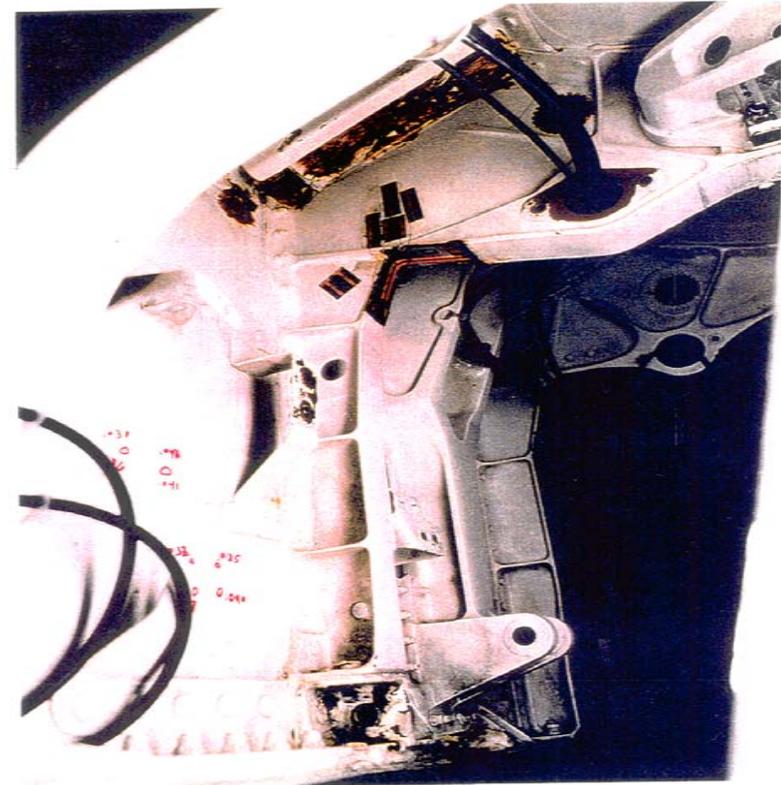


Figure 4.7a Photograph showing the location of the former segment flange radius on bulkhead 497 (L.H.S) and the ACPD probes installed on the location.

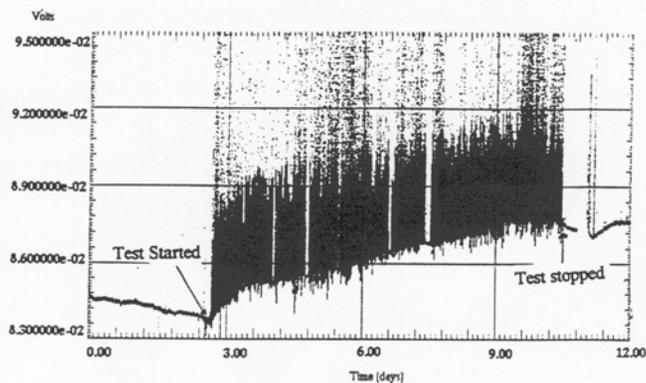


Figure 4.12a Zoom of figure 4.11b.

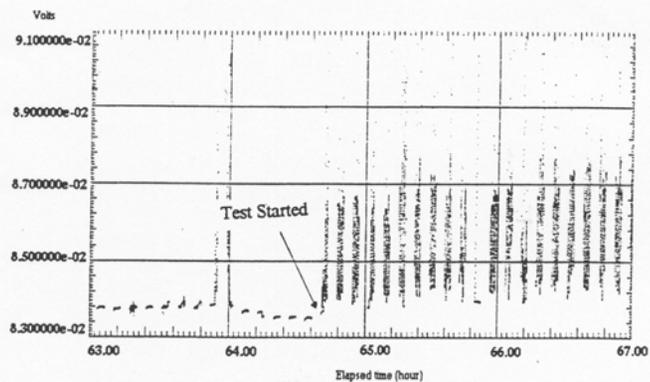


Figure 4.12b Further zoom (63-67 hours) of fig. 4.12a showing the start of block 11.

Instrumentation of F18 bulkheads

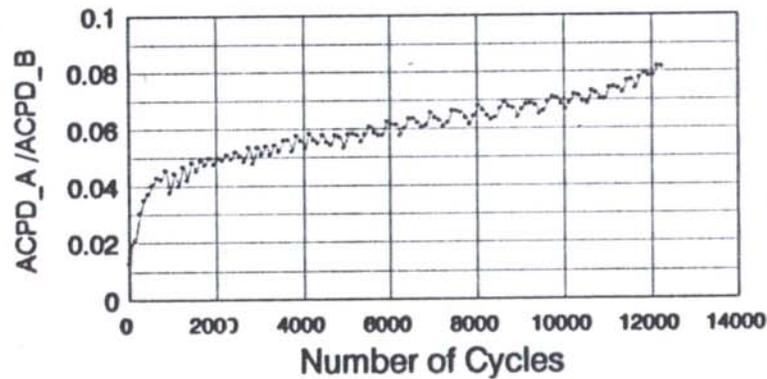
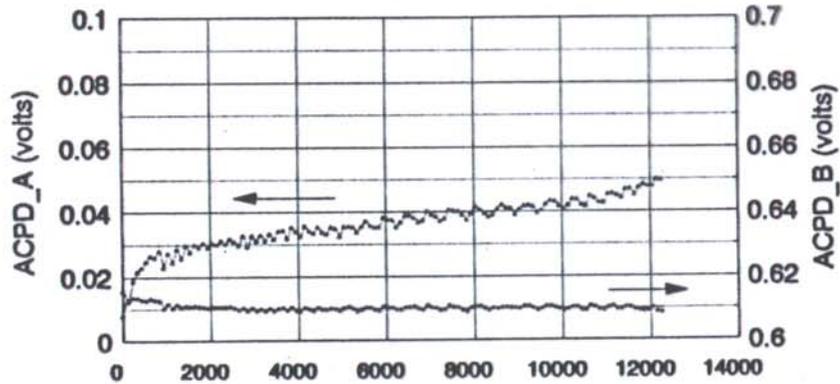
- centerline
- hydraulic hole
- flange radius

Monitor strain and damage during flight spectrum loading

Determine damage during critical maneuvers



- ❑ Crack first detected 2500 SFH prior to other techniques.
- ❑ The crack grew about 415 μm during loading block 11 and 12 (3250-3900 SFH)
- ❑ At 5900 SFH and after 8 complete NDI runs (eddy-current, liquid penetration and ultrasonic) cracks were found in the area indicated much earlier by the ACPD sensors
 - ❑ By 5900 SFH the crack had a surface length of approx. 6 mm with and a depth of approx. 750 μm



ACPD_A --- working probes
ACPD_B --- reference probes

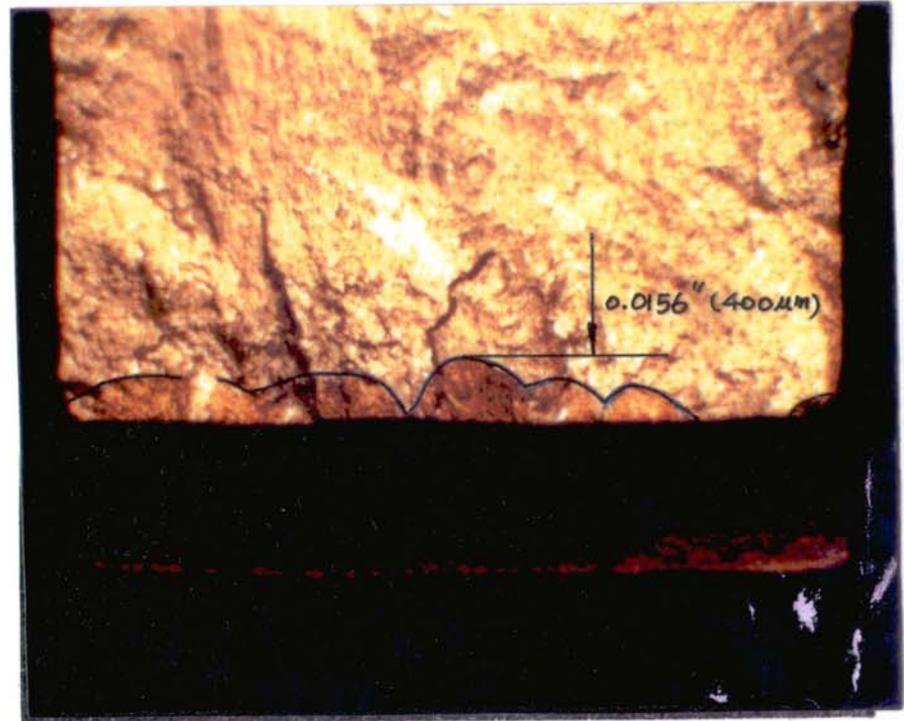
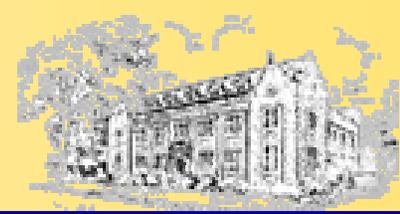
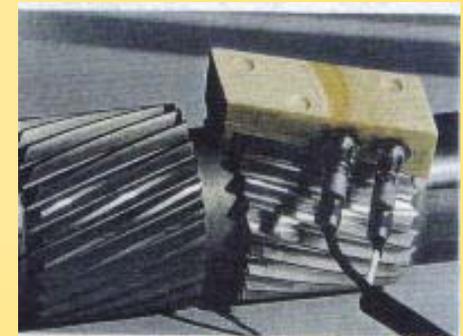
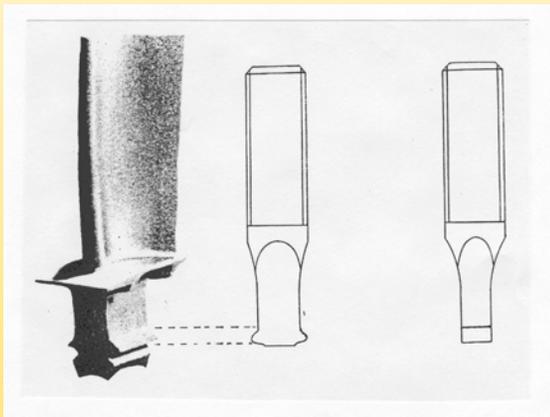


Figure 5. A typical results of ACPD response to multiple fatigue crack initiations at the root of the notch. (Ti64, RT)



- *Residual stresses in metals*
- *Cracks in blades, gears and threaded components*

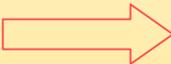




- *Advantages*
 - proven technology - robust and inexpensive sensors
 - durable sensor design (bonded strips and probes)
 - provides details of crack shape
 - very sensitive – can resolve growth increments of 0.010 mm
 - provides real time monitoring of damage state and strain history
 - ideal technology to warn of strain overloads
 - allows detection of *both* crack initiation and growth in any conductive material at any temperature

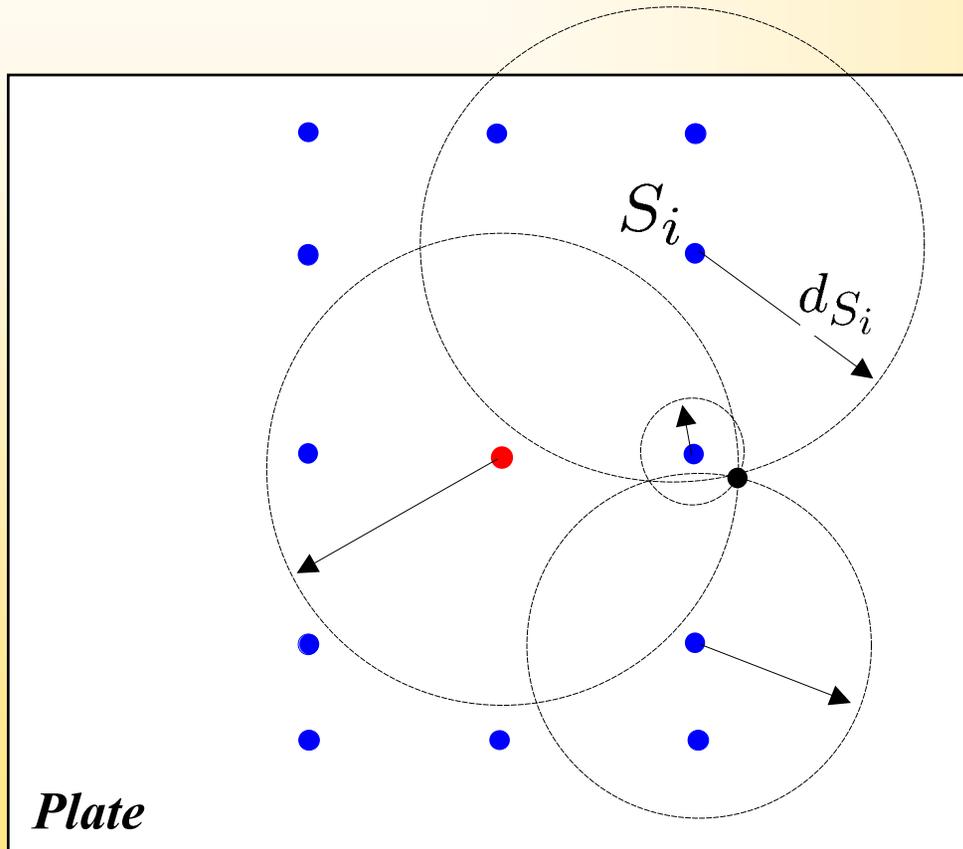
- *Disadvantage*
 - can not be used for composite structures



- *very effective for composites*
- *Previous shortcomings include:*
 - Local sensitivity to defects (need for scanning devices)
 - Limited information regarding precise damage location
 - High sensitivity to noise and vibrations
-  *difficult to apply in a Usage Monitoring Framework*
- *GTech is developing LOCALIZATION and SCANNING strategies – e.g., distributed sensor arrays for in-situ monitoring or scanning laser vibrometer*
- *Studies are supported by simulation tools and state-of-the-art experimental equipment*

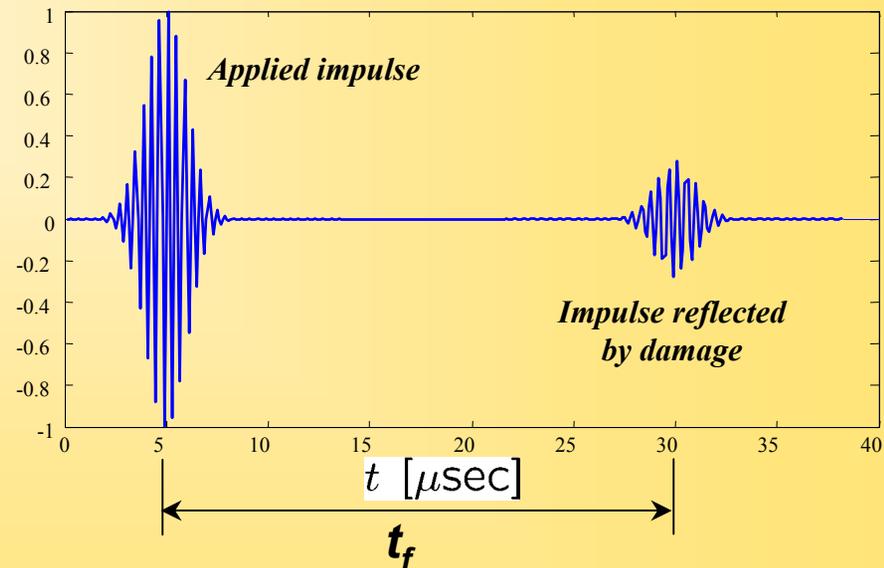


Design of array of sensors for damage localization



- Sensors
- Sensor/actuator
- Damage location

Estimation of "Time of Flight" t_f



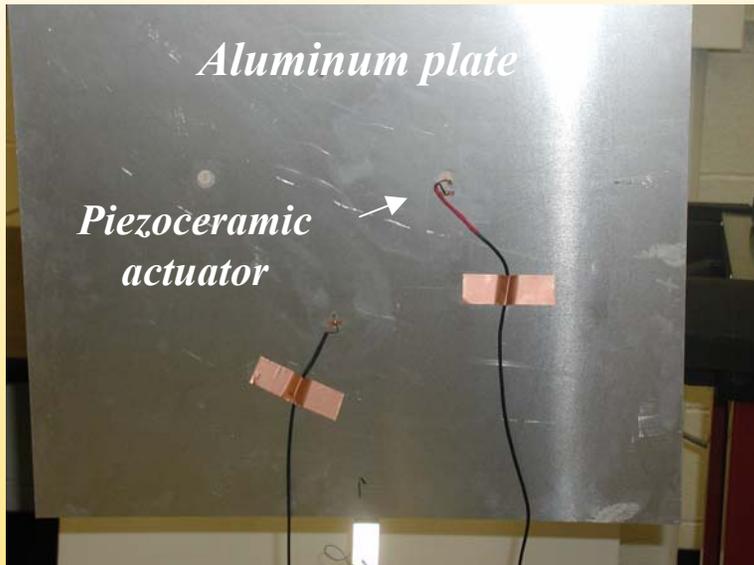
$$d_{S_i} = \frac{c_g}{t_{f_{S_i}}}$$



- Scanning Laser Vibrometer is used to detect and visualize waveforms at low ultrasonic frequencies (25-200 kHz)
- Technique combines ultrasonics sensitivity with scanning laser technology to achieve multi-point detection capabilities
- Distributed (multi-point) measurements directly provide location information for damage
- Technique can be used for:
 - Differential measurements (variation of waveform pattern with damage progression with respect to baseline configuration)
 - CONFIRMATION purposes on grounded rotorcraft
 - Optimization of sensor location and/or
 - Damage analysis and identification in single point ultrasonic measurements



CASE 1: Aluminum plate (thickness=0.0016')



- Aluminum plate excited by a piezo crystal, sinusoidal bursts triggered by vibrometer
- Response at each scanning point is recorded together with required phase information
- Transient response from scanning points is processed to obtain wave propagation information and visualize waveform
- Waveform in a homogeneous plate is first recorded
- Comparison is made with waveform in a plate with discontinuity added (small mass glued to the back of the plate)



Visualization of detected waveforms

Uniform plate

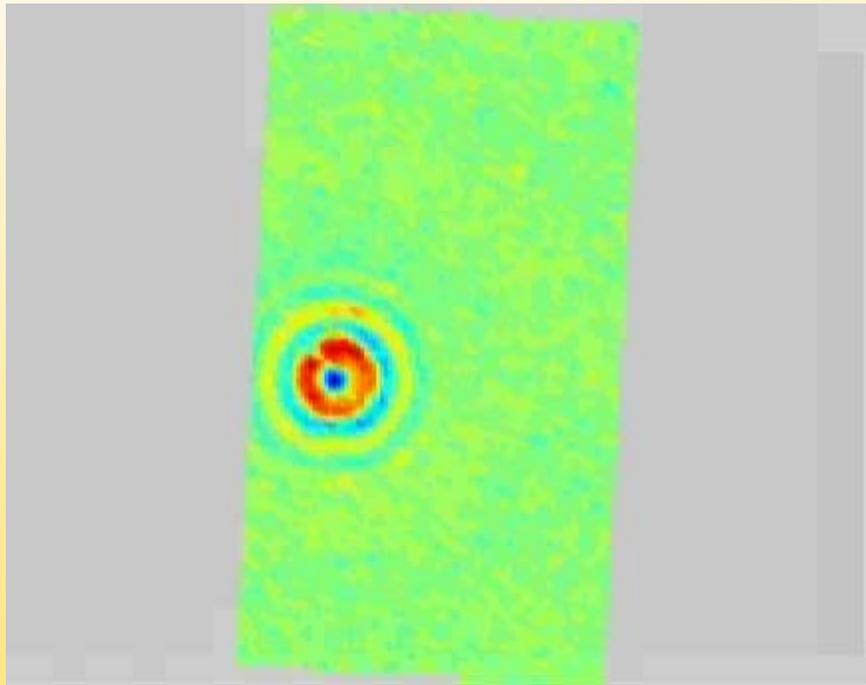
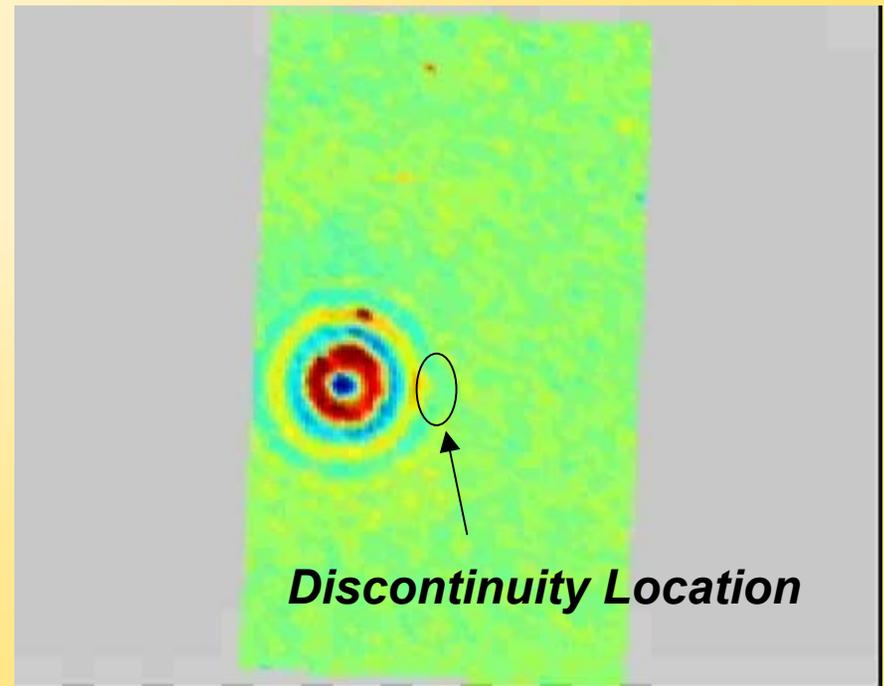
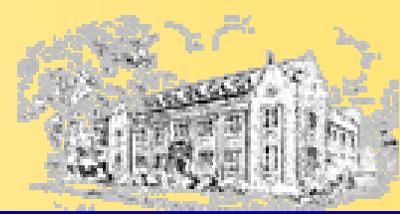


Plate with discontinuity



Excitation: 5-cycle sinusoidal burst at 50kHz



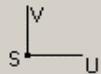
CASE 2: Composite beam with lap joint (0° lay-up, IM7G fiber, 8551-7 Matrix)

Domain Time

Signal Vib Velocity

Time Signal μm/s

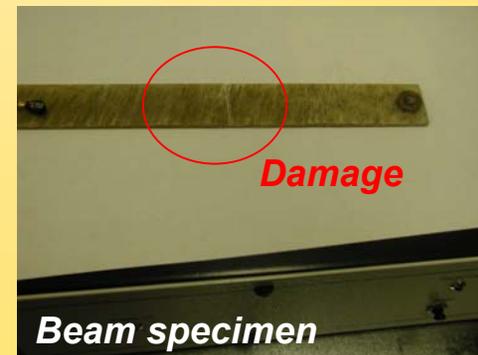
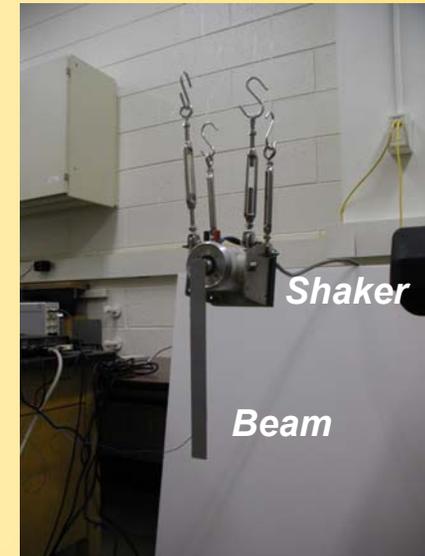
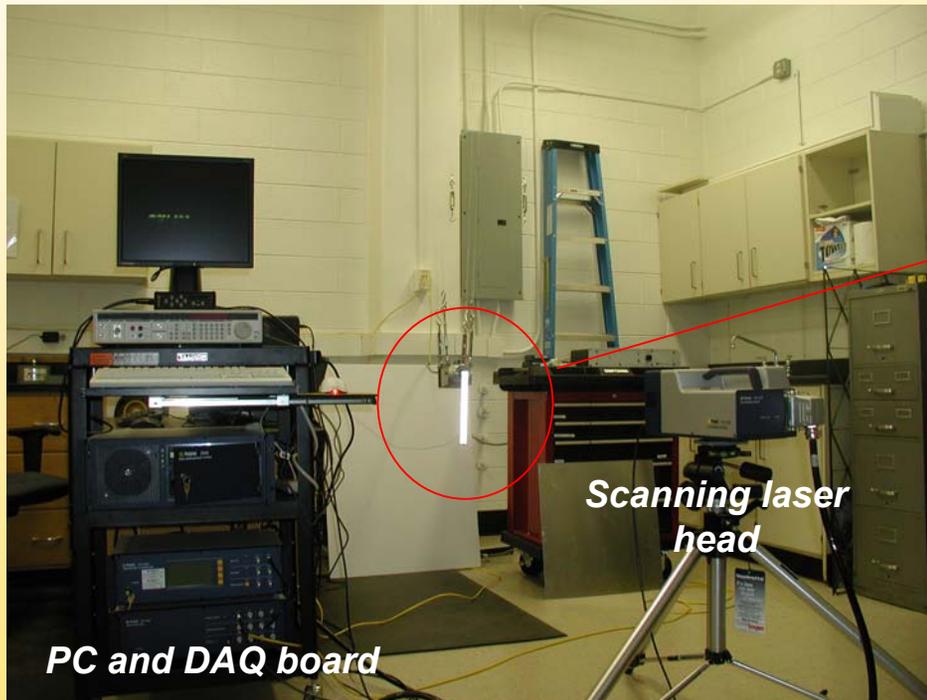
Zoom 438 %



Start	0.00	μs
Current	0.39	μs
End	799.61	μs
Step	1	



Composite beam: experimental setup



*Specimen: 12-ply woven glass and epoxy matrix beam
Damage: Saw cut ~20% of the thickness*



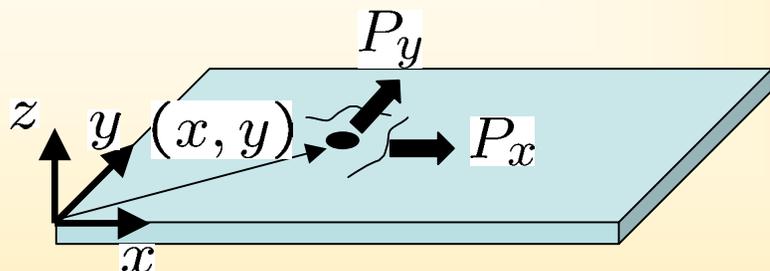
- *Vibrations are “global” damage indicators;*
- *In service vibrations can be continuously monitored;*
- *Previous studies:*
 - Detection of changes in modal parameters (natural frequencies and mode shapes);
 - General low sensitivity, but investigations are limited at low frequencies
 - (100 Hz, GTech looking at up to 10 kHz)
- *Sensitivity can be improved if high frequency (HF) modes are considered;*
- *Energy flow is highly affected by local discontinuities (damage, localized plasticity);*



Evaluation of high frequency energy flows in composite structures



Energy flow at location x, y :



$$P_x(x, y) = \langle F_x(x, y, t) * \dot{v}(x, y, t) \rangle$$

$$P_y(x, y) = \langle F_y(x, y, t) * \dot{v}(x, y, t) \rangle$$

Generalized force

Generalized velocity

- *Energy flow can be measured through:*
 - *Scanning laser vibrometer (Lab setting);*
 - *Embedded distributed sensors (piezoceramics, same as ultrasonics).*

- *Initial studies have been performed on:*
 - *Composite plates*
 - *Cracked composite beams*



Plate results: Amplitude of out-of-plane displacement

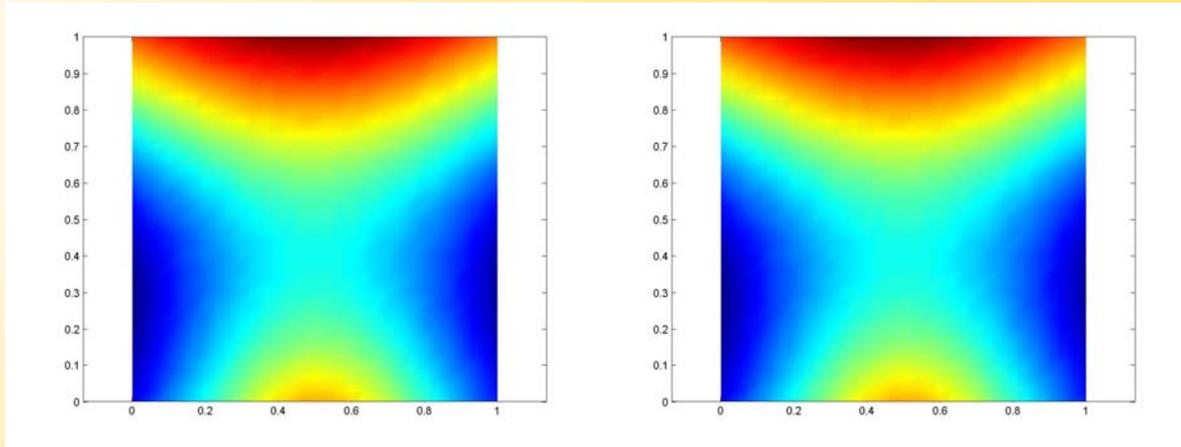
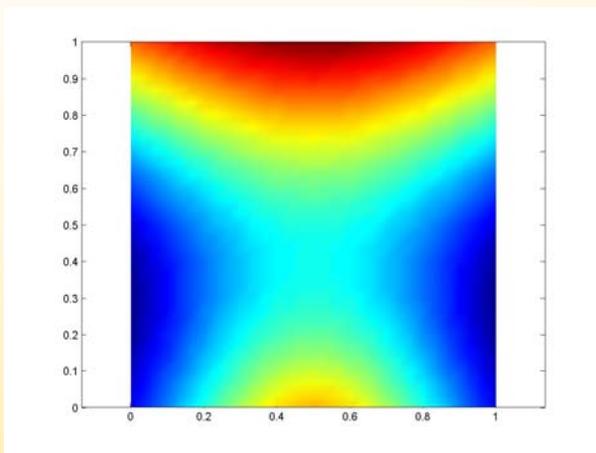
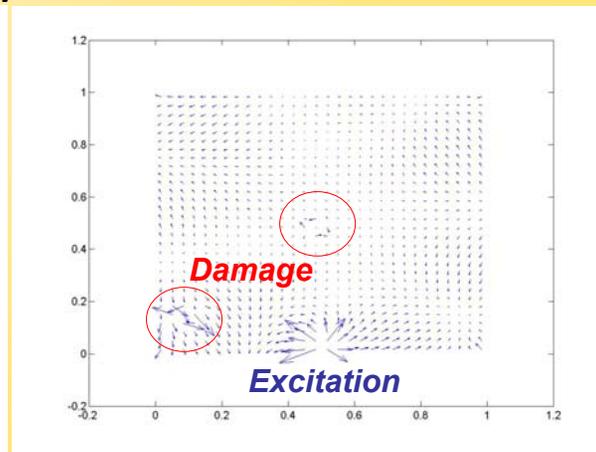
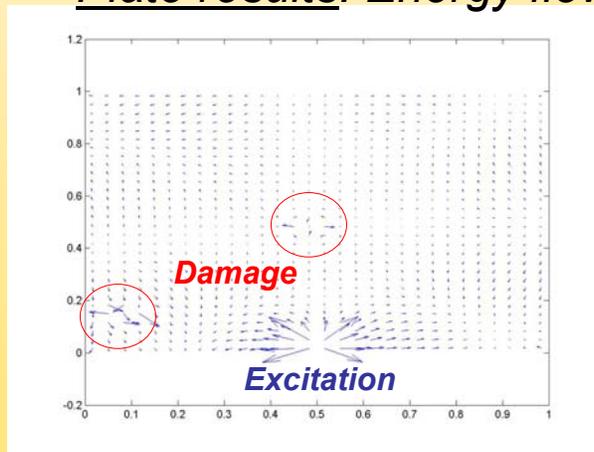
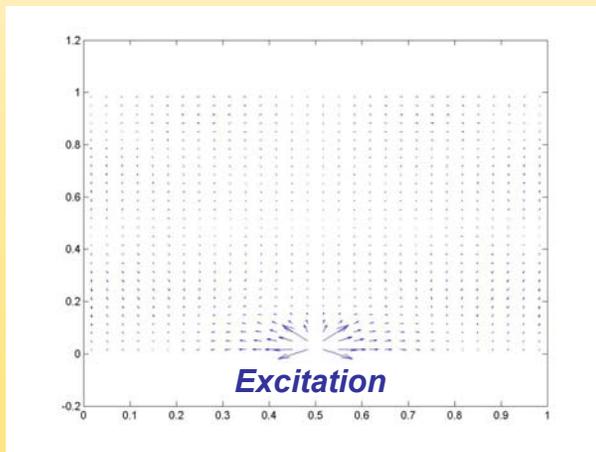


Plate results: Energy flow



Undamaged

10% damaged

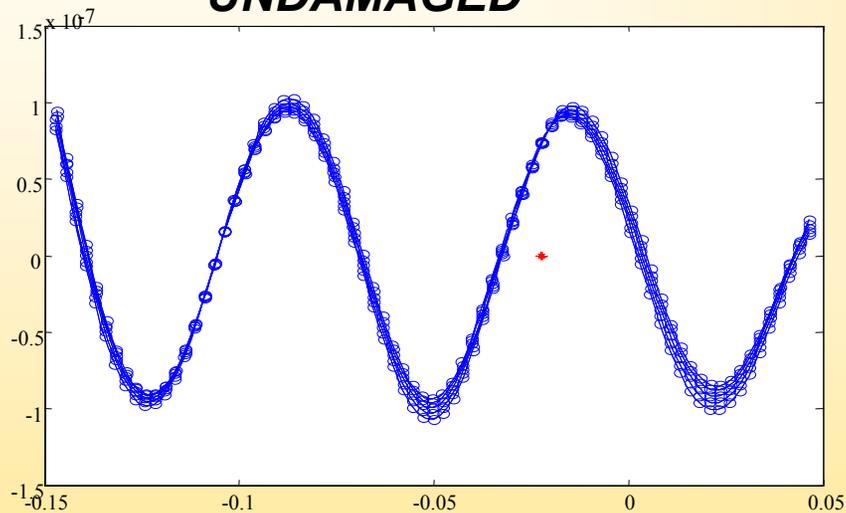
20% damaged

DAMAGE

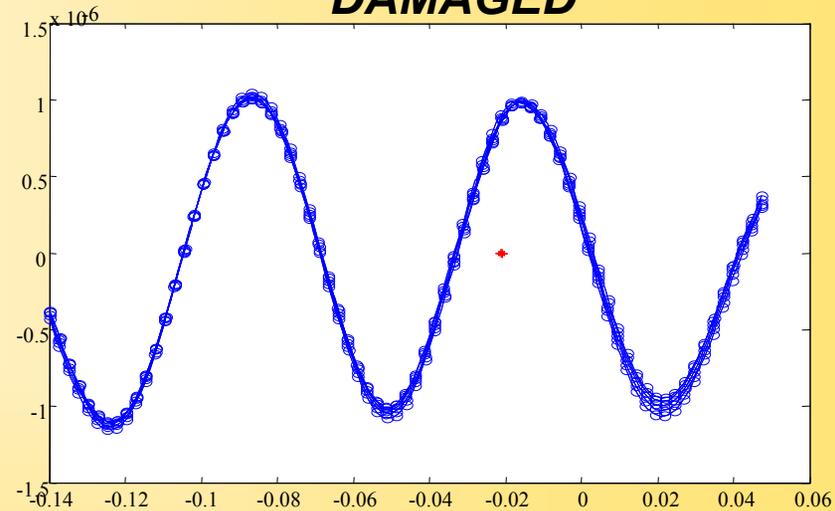


Displacement amplitude @ 1200 Hz

UNDAMAGED



DAMAGED



Energy flow amplitude @ 1200 Hz



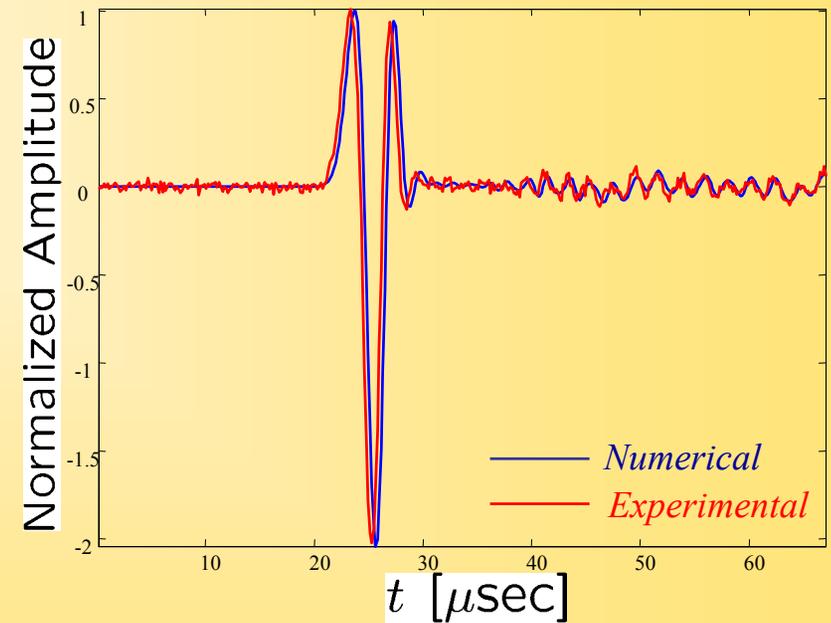
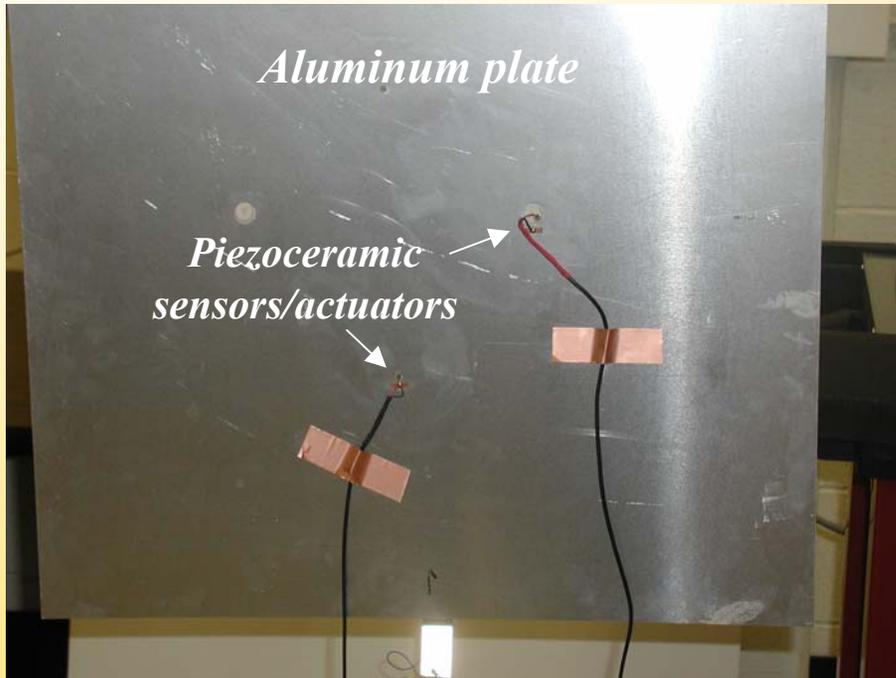
Damage location



- **Modular approach to health monitoring**
 - **ACPD sensor design for metallic components**
 - **Vibration/ultrasonic sensors for composite structures**
 - **Sensor durability and location**
 - **Risk assessment (sensor location and failure)**
 - **Software integration for life prediction**
 - **Validation**
 - **Team with industry**

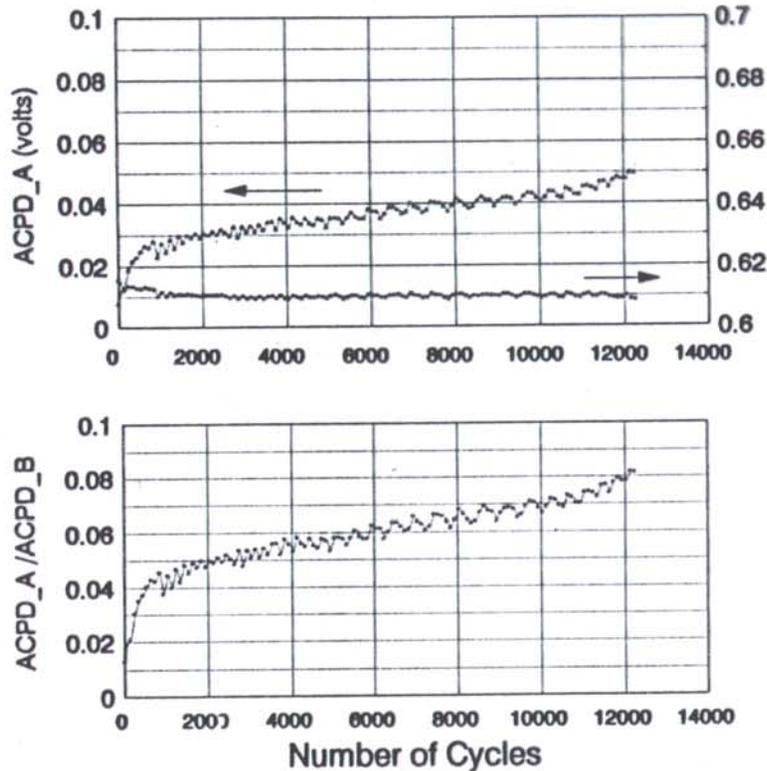


Experimental Validation





ACPD Potential Drop



ACPD_A --- working probes
ACPD_B --- reference probes

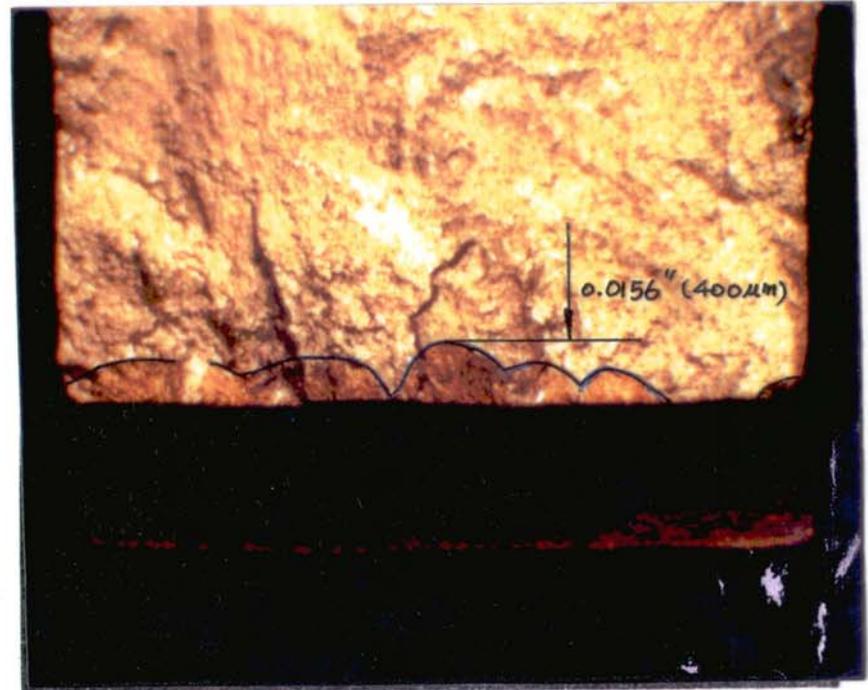


Figure 5. A typical results of ACPD response to multiple fatigue crack initiations at the root of the notch. (Ti64, RT)